

# Improvement of physical modeling for vortex-dominated flows

Project Proposal

Window on Science Seminar

24 September 2018

US Air Force Research Laboratory (AFRL)  
Wright-Patterson Air Force Base, OH, USA

$C^2A^2S^2E$

*DLR, Institute for Aerodynamic and Flow Technology*

German Initiative – DLR, AFRL, AFOSR, Germany, NATO

Project Proposal: *Improvement of physical modeling for vortex-dominated flows*



Wissen für Morgen



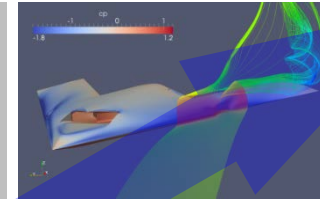
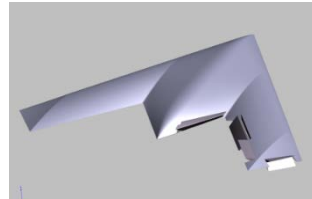
# Background

Requirements from the German MoD and Procurement Agency (BMVg/BAAINBw) with respect to DLR's military research funding:

- ***Sustainment and improvement of capabilities to design, layout and assess the performance of military areal vehicles***

## FaUSST (2011-2013)

- Preliminary overall design
- Generic UCAV configuration, round leading edges & control devices



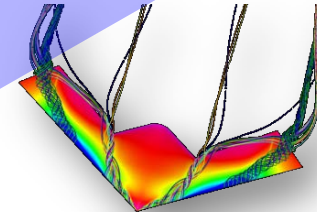
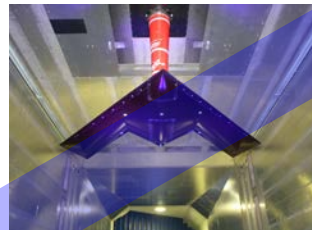
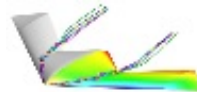
## Mephisto (2014-2018)



- Multi-Fidelity overall design

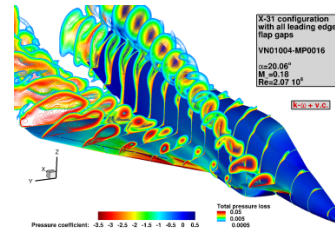
## UCAV-2010 (2007-2010)

- Maneuver simulation
- UCAV configuration, round leading edges
- Flight trajectory simulation



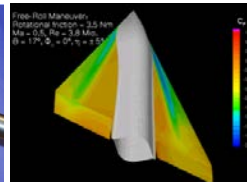
## SikMa (2003-2006)

- Maneuver simulation
- Real configuration, round leading edges



## AeroSUM (1998-2003)

- Maneuver simulation
- Delta wing, sharp leading edge



- Continuous activities over 20 years
- Funding strongly limited



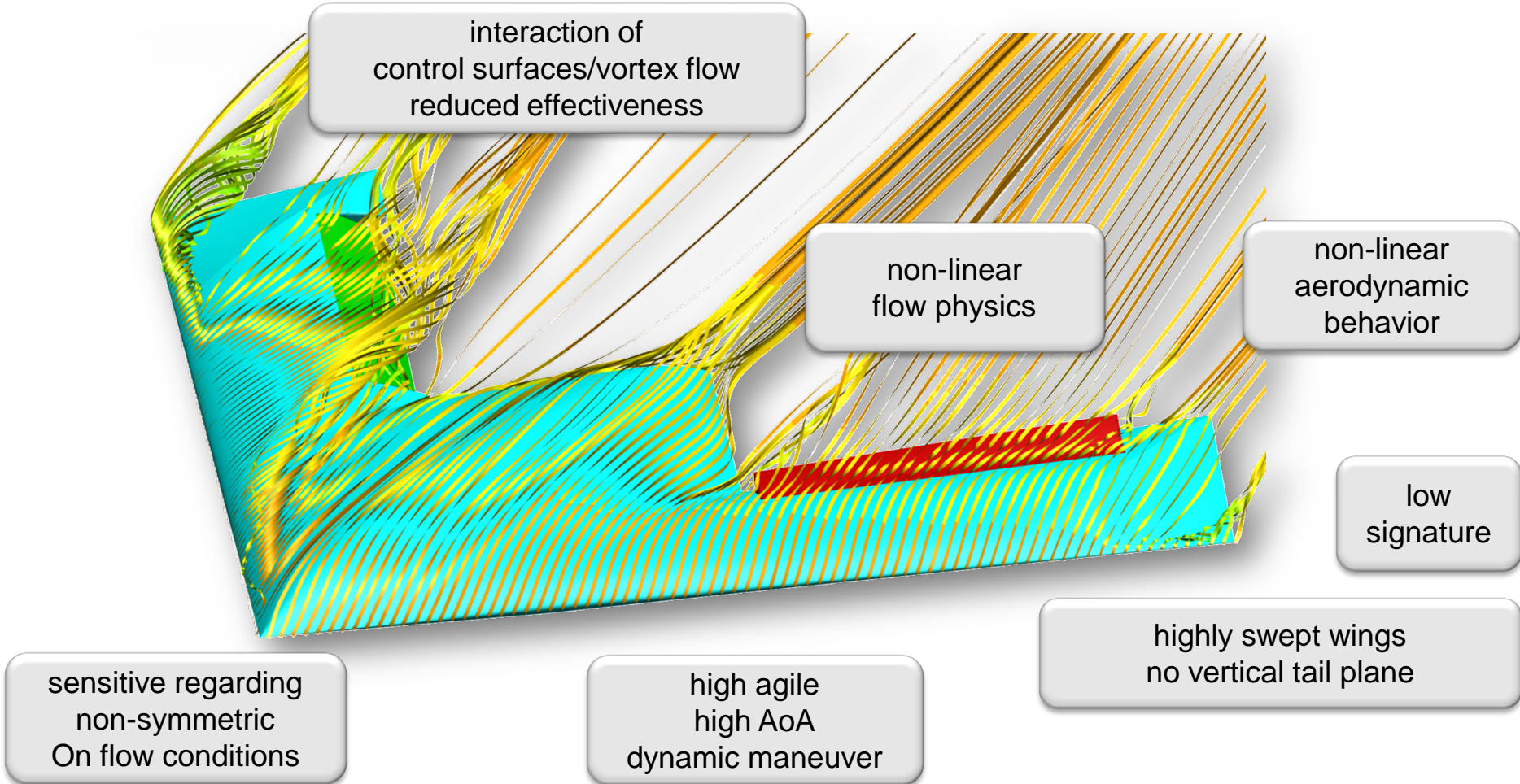
Chart: A. Schütte





# Motivation/Challenges for our institute

Consolidation of design capabilities for agile, low observable military configurations with vortex-dominated flow physics



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Consolidation of design capabilities for agile, low observable military configurations with vortex-dominated flow physics

interaction of  
control surfaces/vortex flow  
reduced effectiveness

- Large number of simulations done
- Driven by practicability considerations, not much space for trying new models
- Very limited testing of advanced modeling approaches
- No systematic investigation of advanced approaches done until now

**This project would be the opportunity.**

non-linear  
flow physics

non-linear  
aerodynamic  
behavior

low  
signature

highly swept wings  
no vertical tail plane

sensitive regarding  
non-symmetric  
On flow conditions

high agile  
high AoA  
dynamic maneuver



Chart: A. Schütte





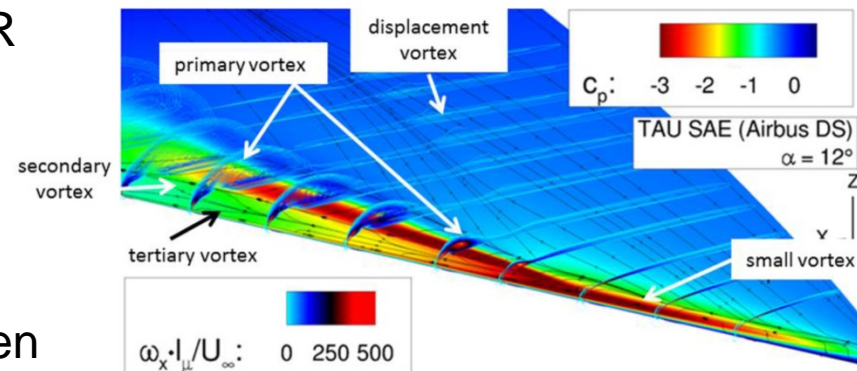
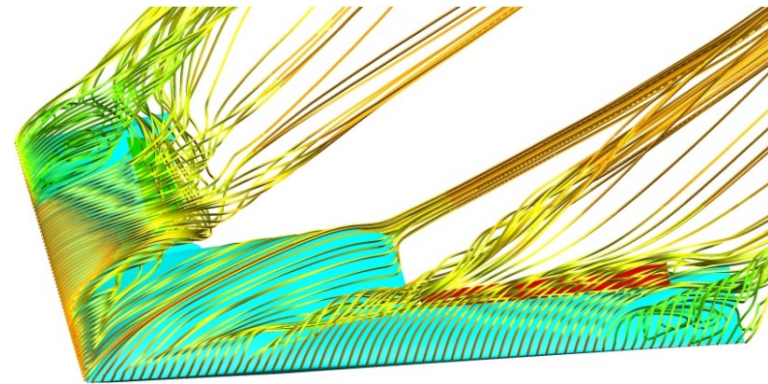
# Proposal of a research project over 3 years

## Current situation:

State-of-the-art CFD methods lack the ability to predict onset and progression of separated vortex-dominated flows, ***especially from smooth surfaces***

## Approach:

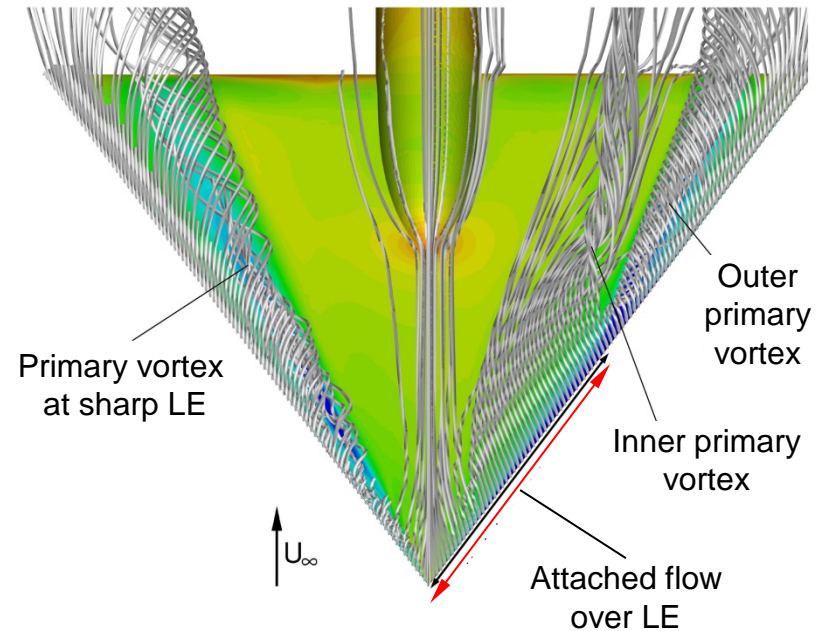
- Evaluation and enhancement of innovative turbulence modeling approaches including both advanced RSM and SRS approaches recently developed at DLR
- Investigations will be carried out using the DLR TAU code
- Test cases to be carefully selected by DLR and AFRL
- Information exchange intended between DLR, AFRL and Airbus Defense and Space



# Proposal of a research project over 3 years

## Not yet solved:

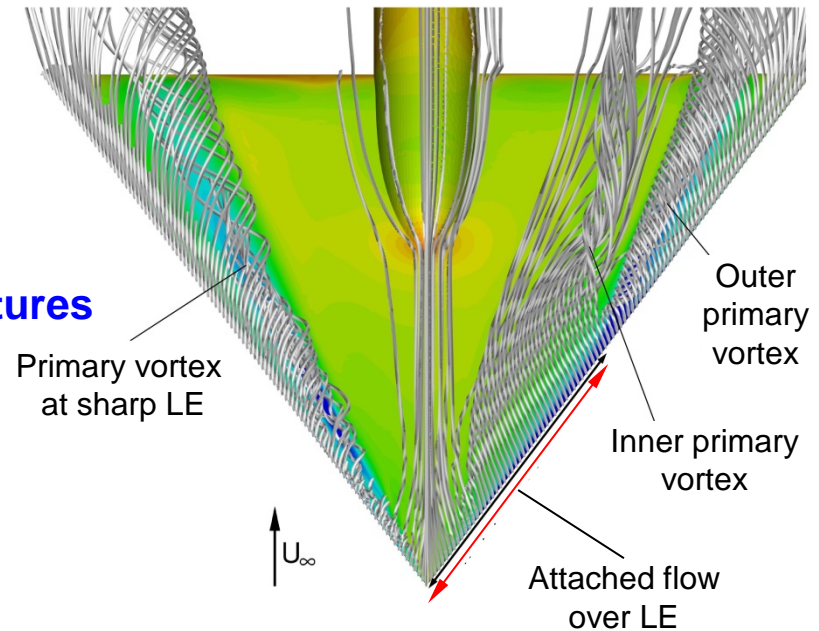
- Correct prediction of complex vortex structures
  - Secondary vortex separation
  - Multiple vortex structures



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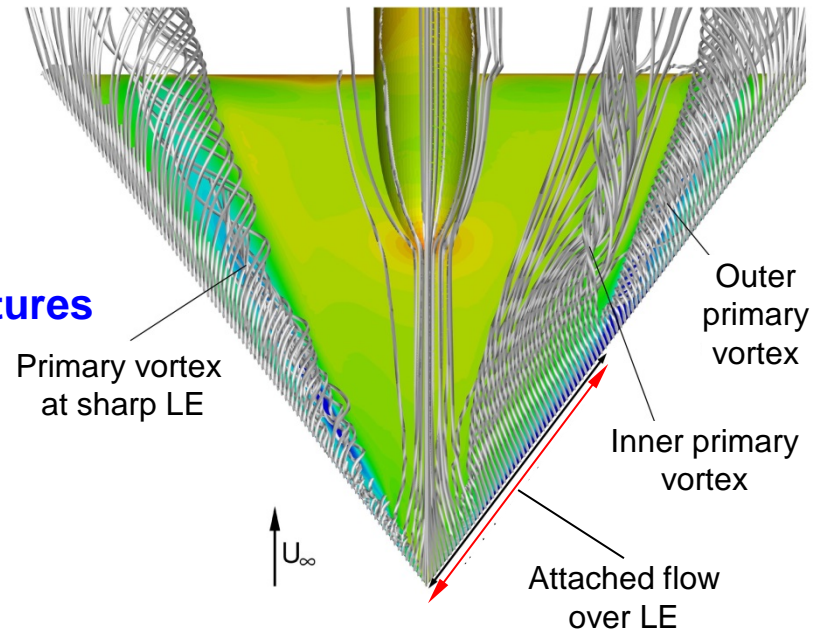
- Correct prediction of complex vortex structures → **RSM**
  - Secondary vortex separation
  - Multiple vortex structures
- **good representation of rotational flow features**
- **existence and location of vortices**



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- Correct prediction of the vortex strength

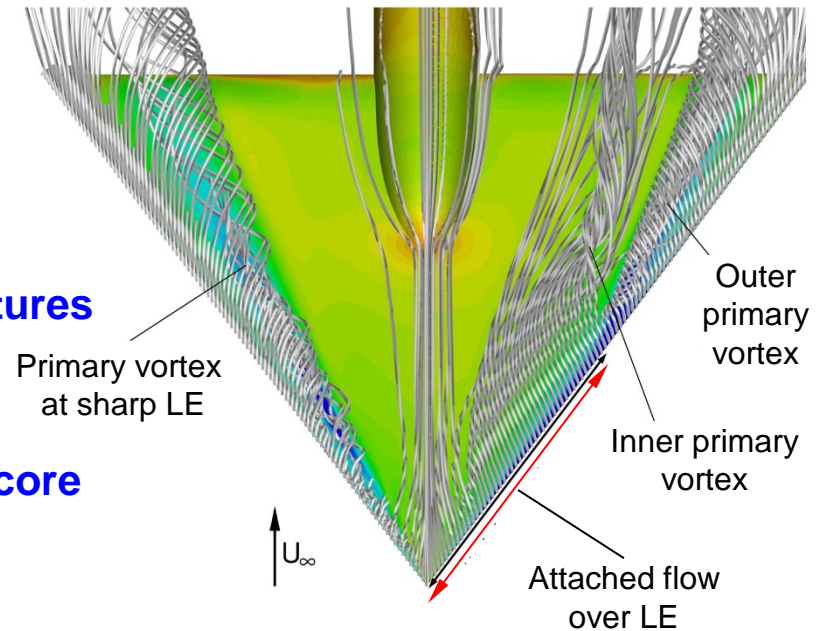




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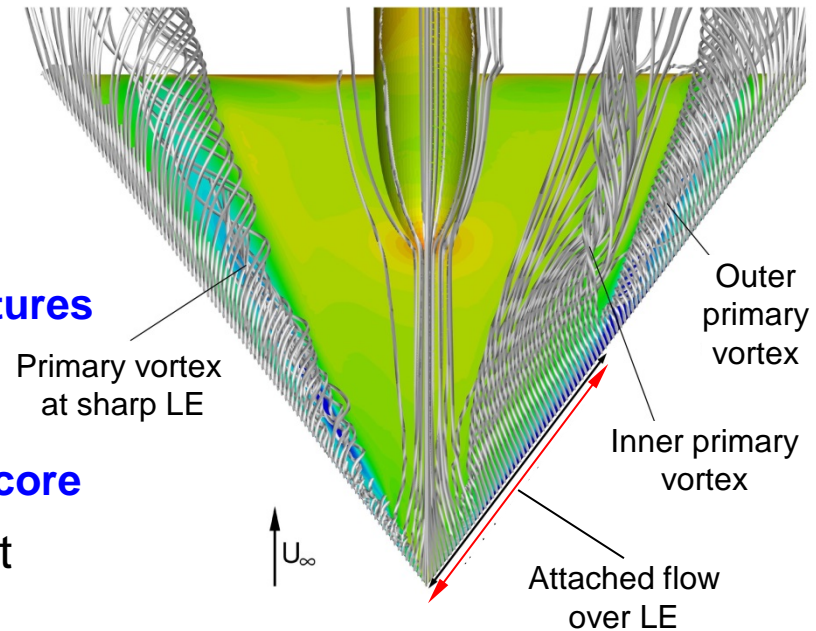
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- Correct prediction of the vortex strength  
→ **RSM: better prediction of wing-tip vortex core**



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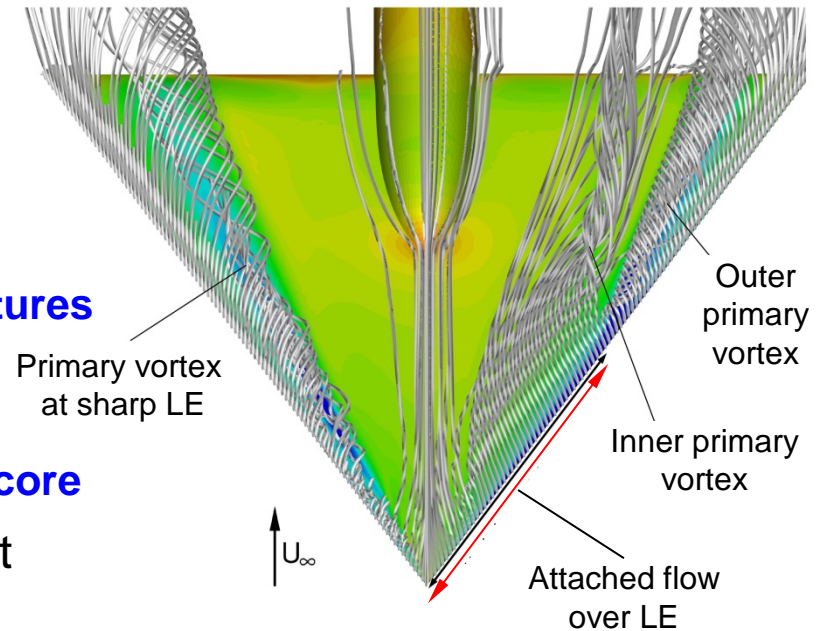
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- Reliable prediction of the vortex onset point location  
→ **RSM: better separation onset locations in APG TBL possible**

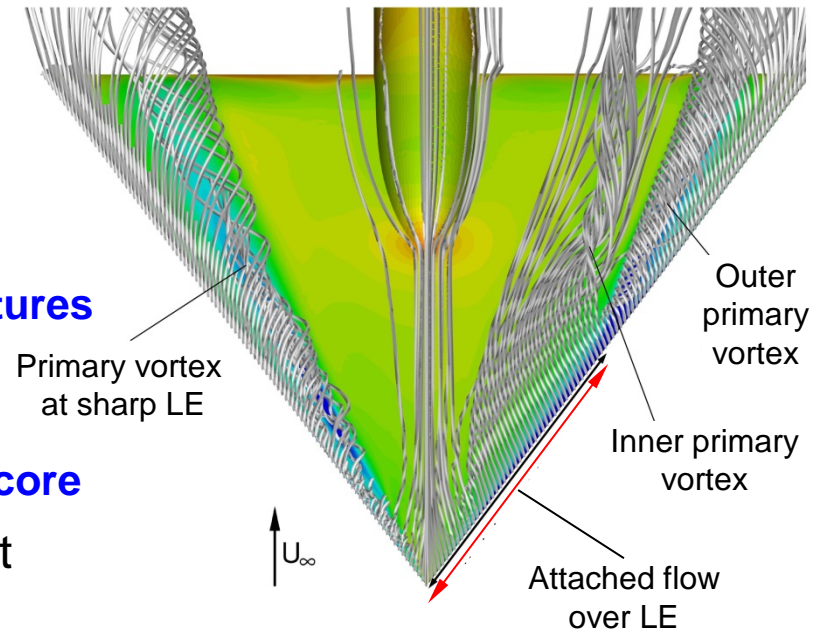




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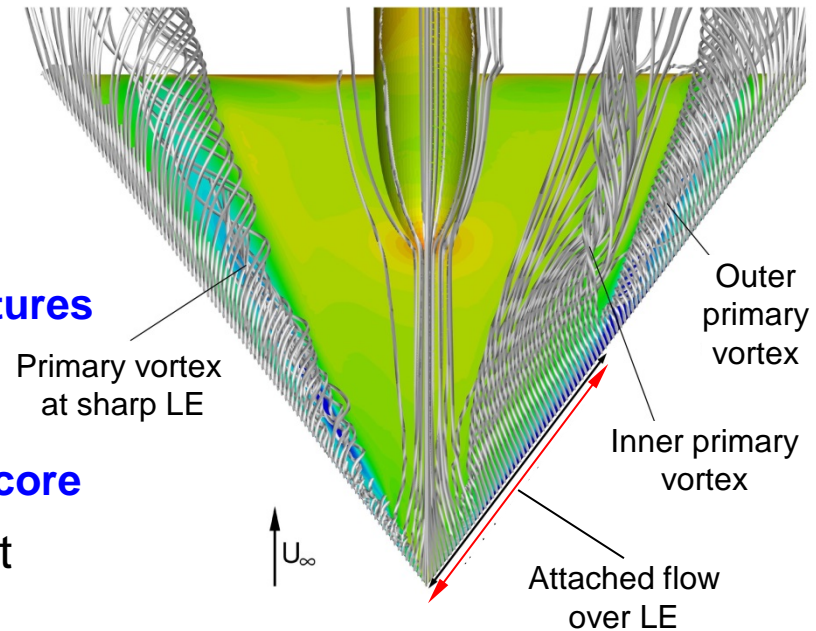
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  - **RSM: better separation onset locations in APG TBL possible**
  - **SRS: might be necessary**



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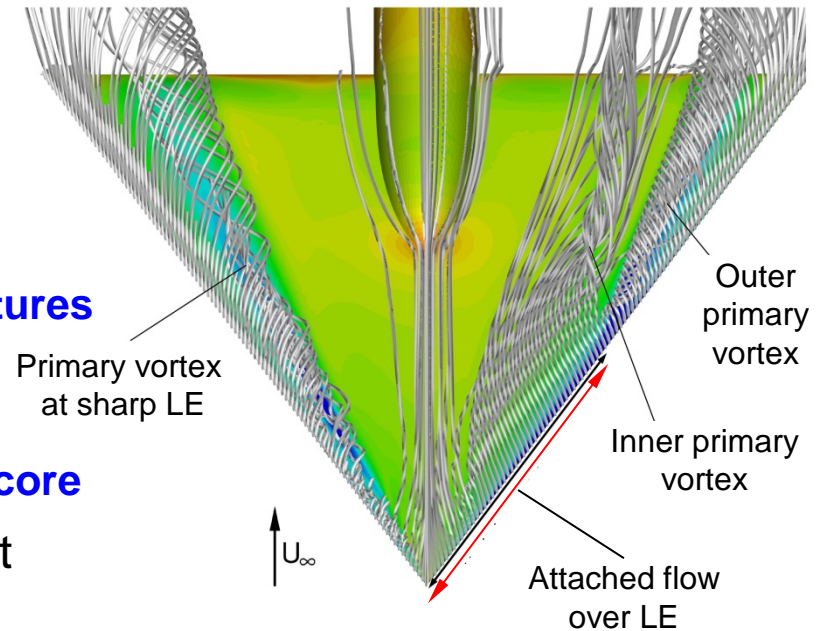
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- Reynolds number effects have been hardly taken into account so far



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## Still work to be done:

- Reliable prediction of vortex burst point

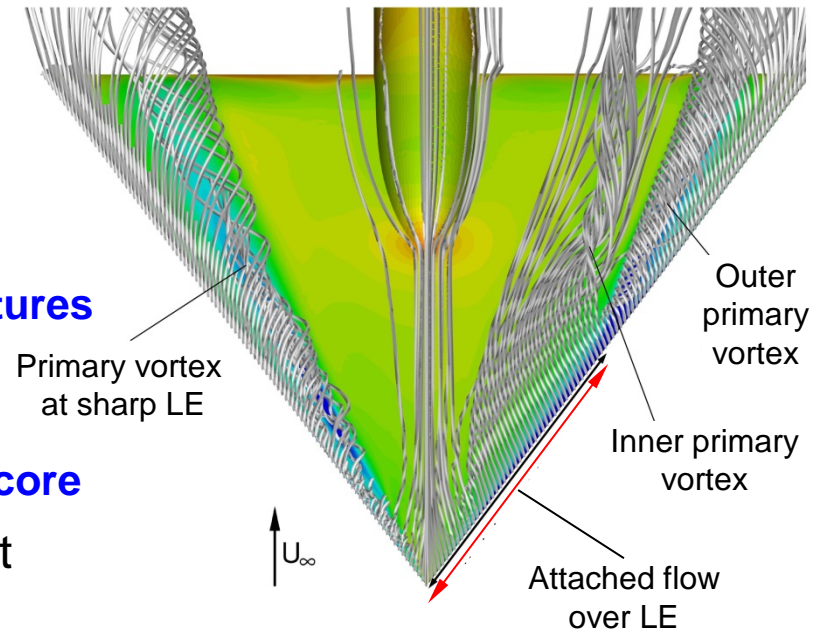




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## Still work to be done:

- Reliable prediction of vortex burst point  
→ **SRS probably necessary: highly unsteady!**



# WP 1: Computation of selected test cases using SSG/LRR-RSM

- Selection of test cases: DLR + AFRL → Cases with round leading edges
- Generation of appropriate computational grids
- Simulations using SSG/LRR Reynolds stress model
  - Model variant of the standard RSM in TAU: SSG/LRR- $\omega$
  - Alternatively, use of  $g$  or  $\ln(\omega)$  formulation of model → Higher numerical stability
- Grid study: refinement, cell types (hexahedral?), ...
- Investigation of Reynolds number effects
- Comparison with experimental data
- Additional computations with a eddy-viscosity model → Which? Decision at project runtime

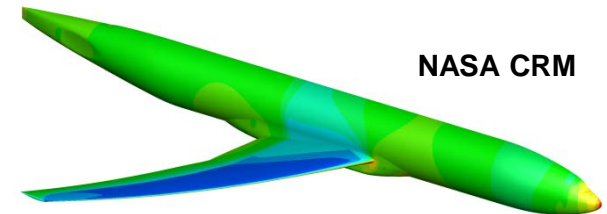
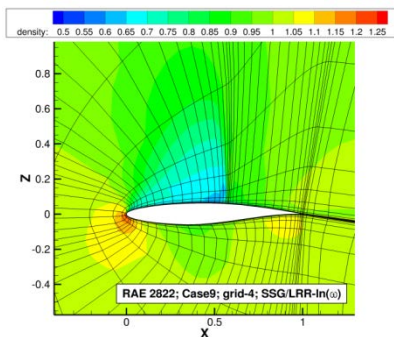
- Goals:**
- Assessment of predictive capability of SSG/LRR-RSM for separated vortex-dominated flows → Is RSM sufficient?
  - Application recommendations, Best Practice



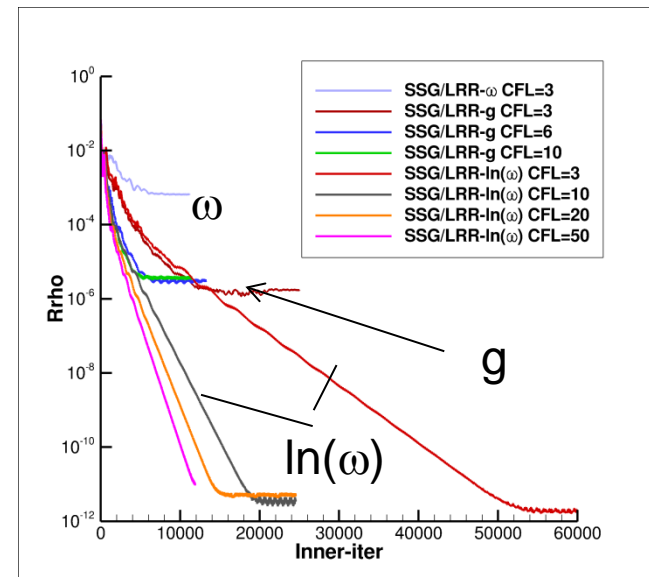
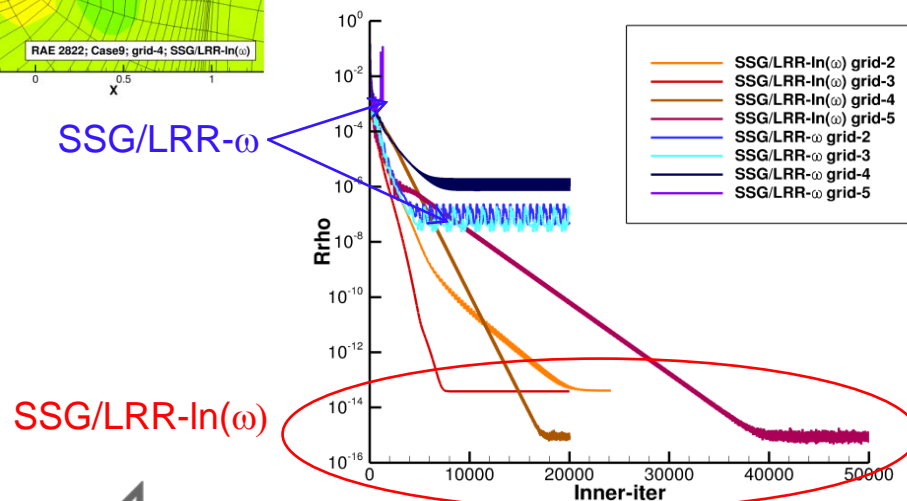
# SSG/LRR-RSM with different length-scale formulations

- The model is identical with all formulations of the length-scale equation
- Results (almost) identical if grids are fine enough (identical, if grid convergence achieved)
- Numerical stability of  $\omega < g < \ln(\omega)$
- With  $\ln(\omega)$  results towards machine-accuracy possible

RAE 2822 airfoil



RAE 2822; Case 9; CFL=15; 3v-Multigrid

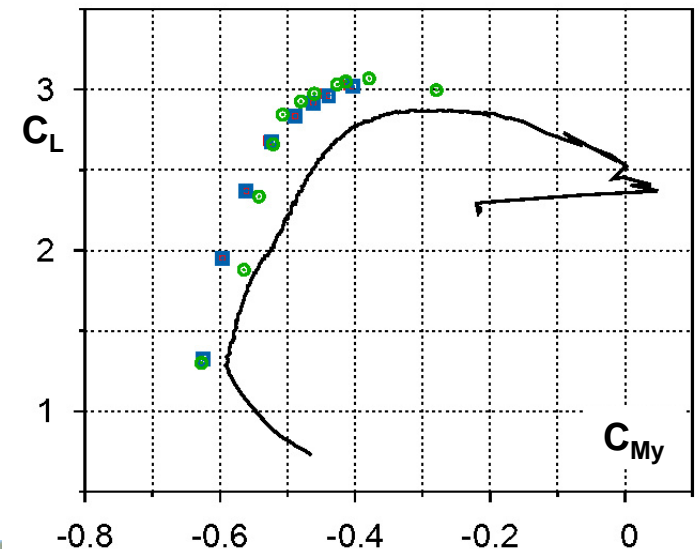
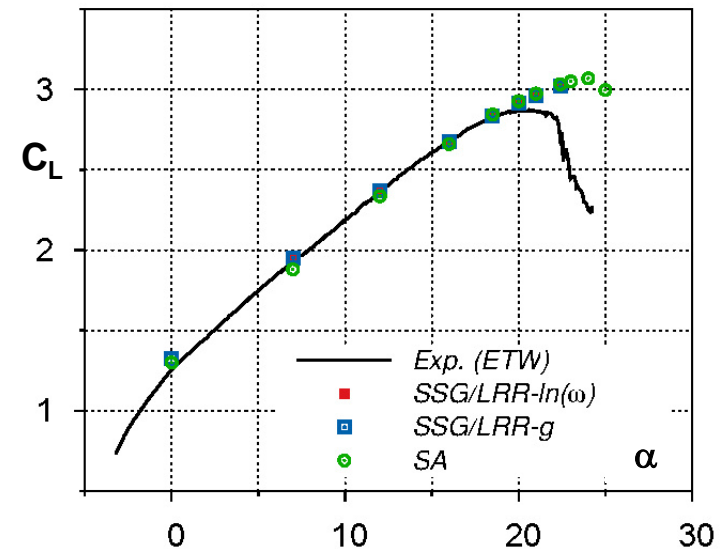




# SSG/LRR-RSM with different length-scale formulations

- For DLR-F11:  $Re_{MAC} = 15 \times 10^6$ ,  $Ma = 0.175$ 
  - SSG/LRR- $\omega$  fully unstable  $\rightarrow$  **no results**
  - SSG/LRR- $g/\ln(\omega)$   $\rightarrow$  similar residual levels, with  $\ln(\omega)$  higher convergence rates

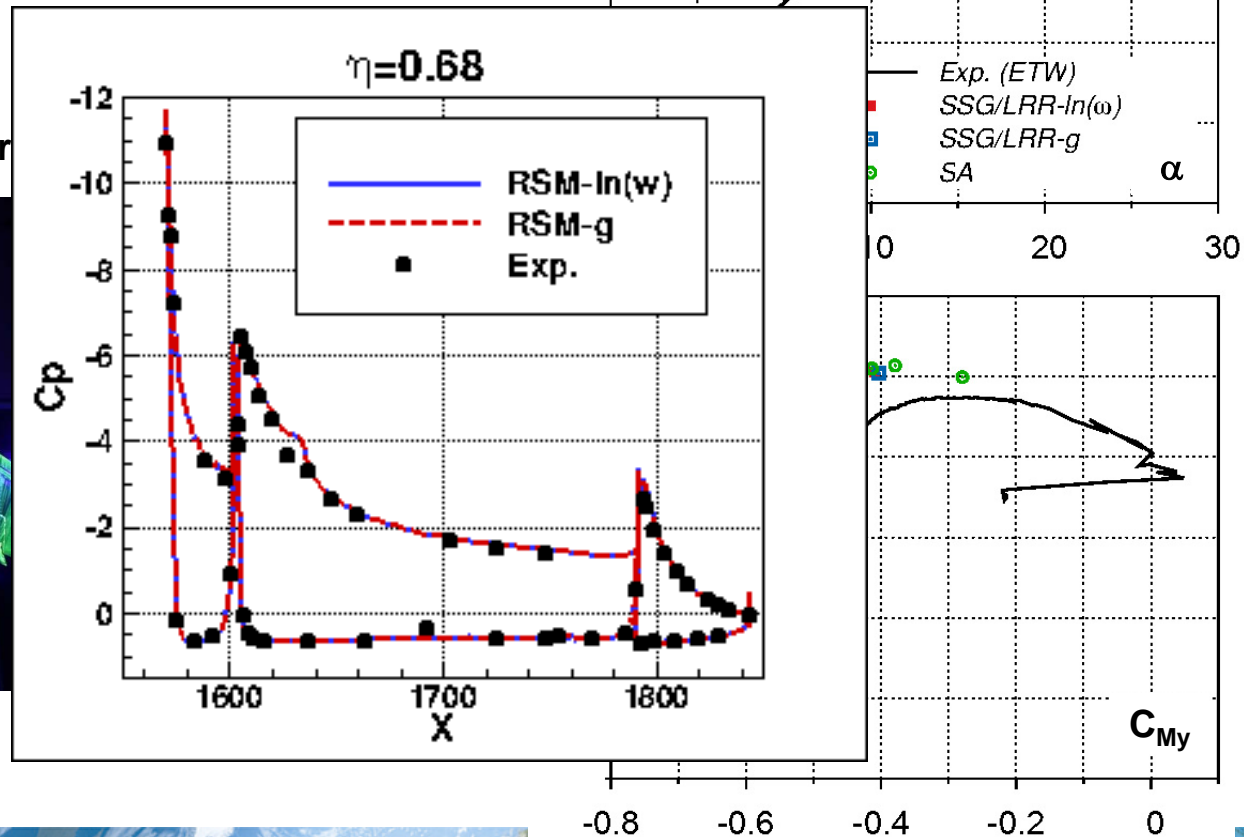
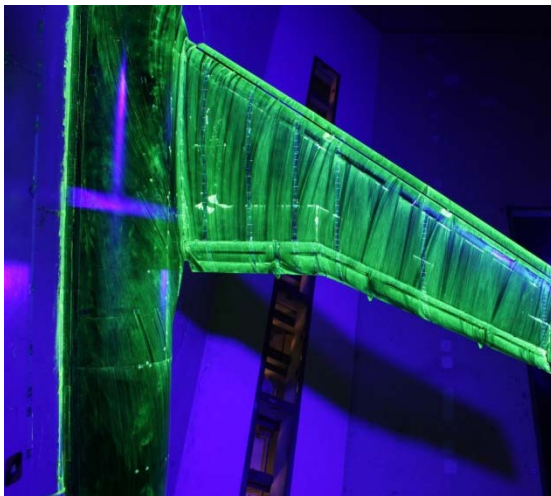
DLR-F11 high-lift configuration



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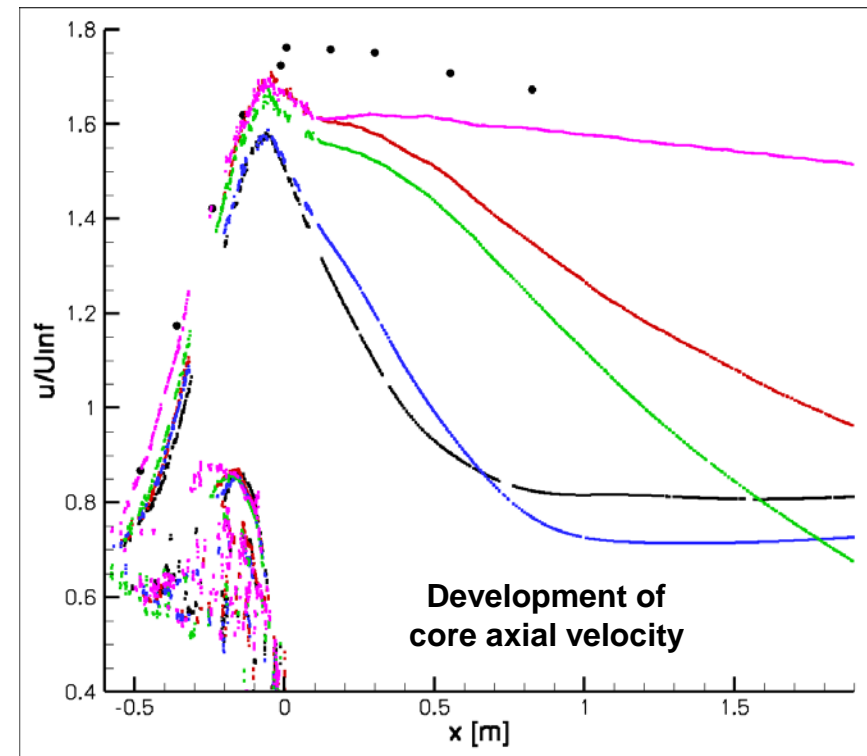
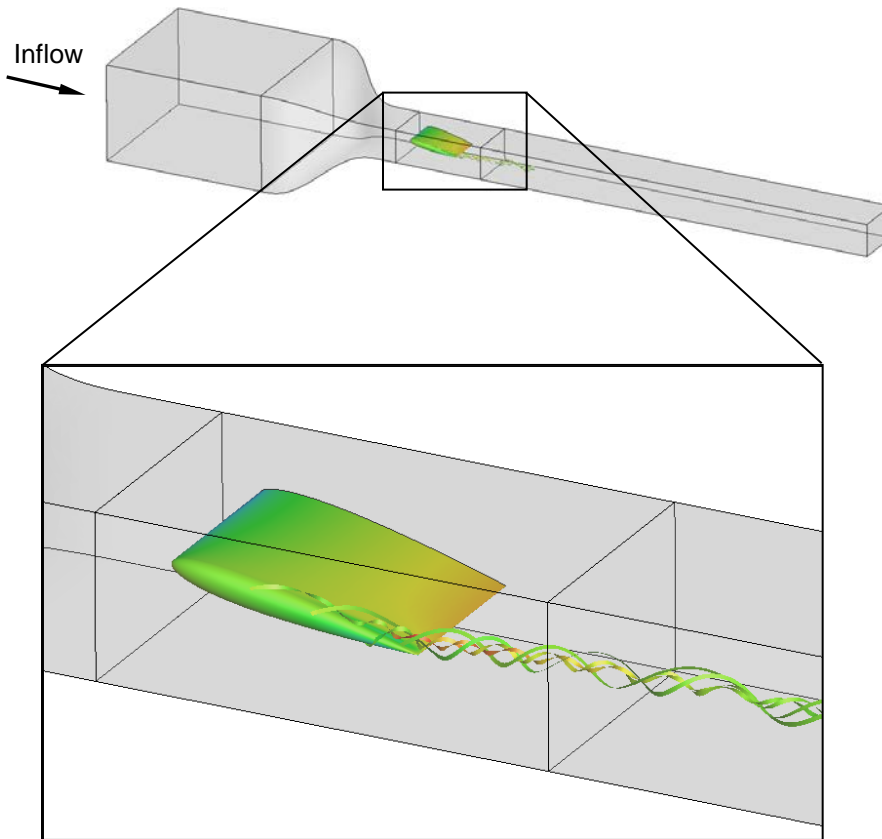
DLR-F11 high-lift configura



# Simulation of vortices after separation from smooth surfaces

- **Test case:** NACA0012 Wing Tip Vortex at  $\text{AoA} = 10^\circ$ 
  - Measured in 32x48 inch low speed WT at NASA Ames Research Center

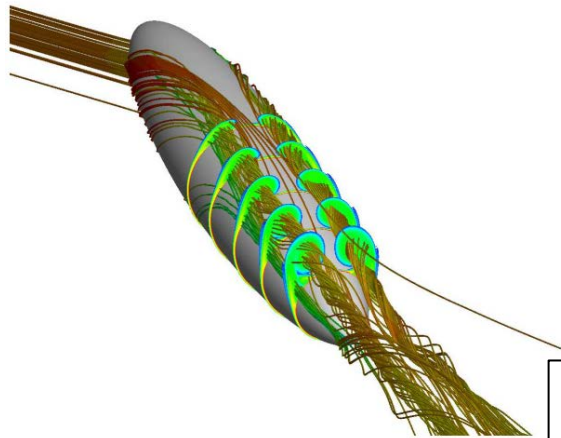
- Exp.
- SST, Airbus set., Mesh 3, Roe2nd
- SST.NLR, Airbus set., Mesh 3, Roe2nd
- SST, DLR set., Mesh 3, Roe2nd
- SST.NLR, DLR set., Mesh 3, Roe2nd
- RSM, Roe2nd





# Simulation of vortices after separation from smooth surfaces

- **Test case:** Prolate Spheroid
  - $Re = 4.2 \times 10^6$ ,  $Ma = 0.2$ ,  $AoA = 20^\circ$  at NASA Ames Research Center
  - $61 \times 10^6$  grid points (mostly hexahedral)

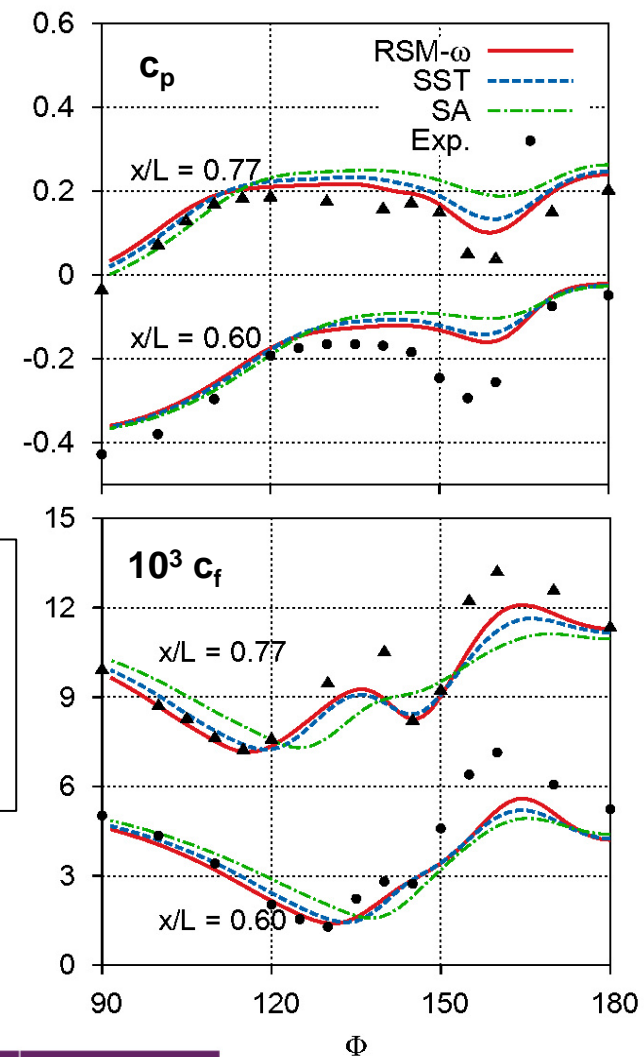
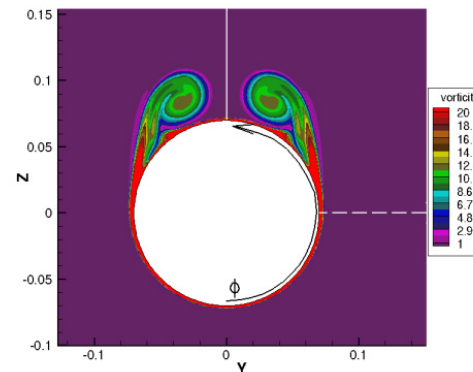
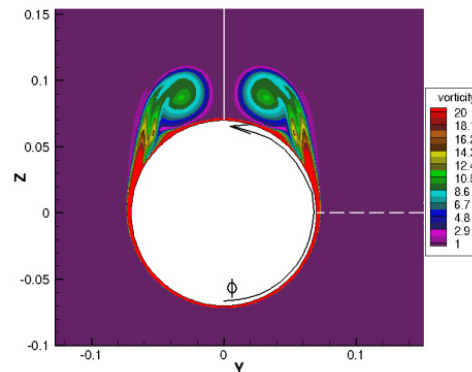
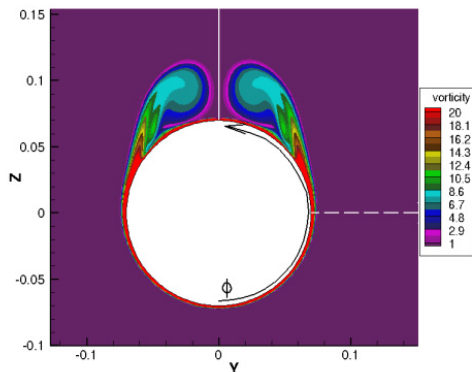


**Too weak interaction of vortex and BL lead to incorrect local  $c_p$  peak at  $\Phi \sim 155^\circ$**

- Finer grid in boundary layer
- For EVMs application of vortex corrections

**Vorticity contours at  $x/L = 0.77$**

- weaker with EVM



## WP 2: Computations using selected SRS approaches

- Computations of some (selected) cases of WP1
  - Selection of appropriate SRS approaches
    - Based on the results and findings from WP1
    - Taking into account latest achievements and results of other ongoing activities at DLR
    - Hybrid RANS/LES, e.g. DDES, IDDES, ADDES → Decision at project runtime
      - SGS: SA, SST → Decision at project runtime
  - Generation of appropriate computational grids (preferably derived from WP1)
  - Comparison with experimental data and results from WP1
- Goals:**
- Clarification in which flow situations RSM is sufficient or if SRS is necessary to predict the flow over a specified configuration
  - Clarification which SRS approach is the appropriate (most appropriate) one
  - Application recommendations, Best Practice



# Hybrid RANS/LES results for VFE-2 Delta Wing at $\alpha = 23^\circ$

Sharp Leading Edge

**Unstructured grid** from Airbus-DS:

- „industrial“ prism/tetra grid
- 17.5 million points

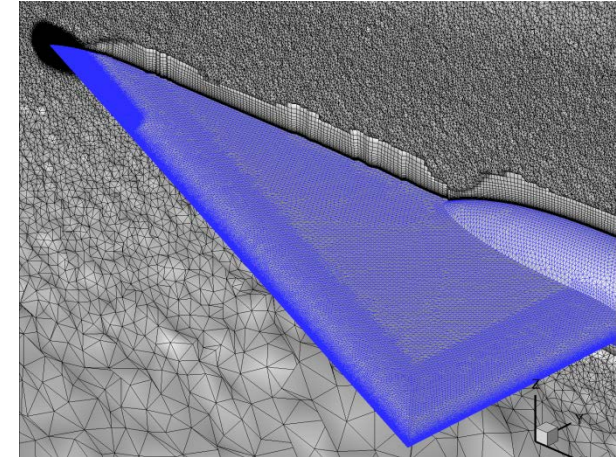
**Numerics:**

- DLR-TAU code
- assessment of hybrid LD2 (HLD2) scheme  $\rightarrow$  active only in LES regions

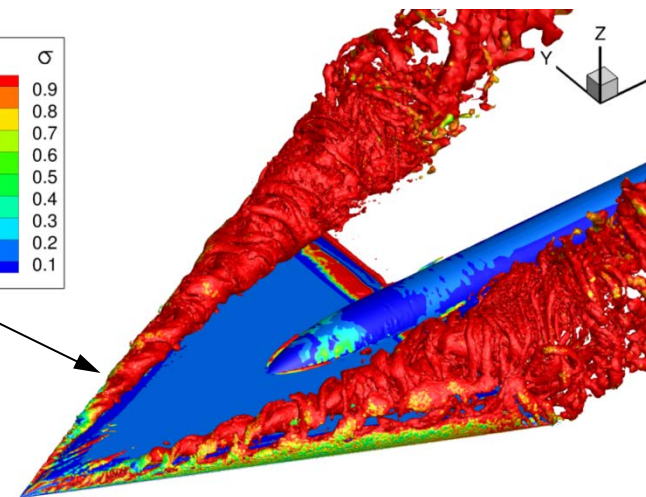
**Model:** SST-DDES

**Temporal settings:**

- time step:  $3.75 \cdot 10^{-4}$  CTU
- total time: 11 CTU

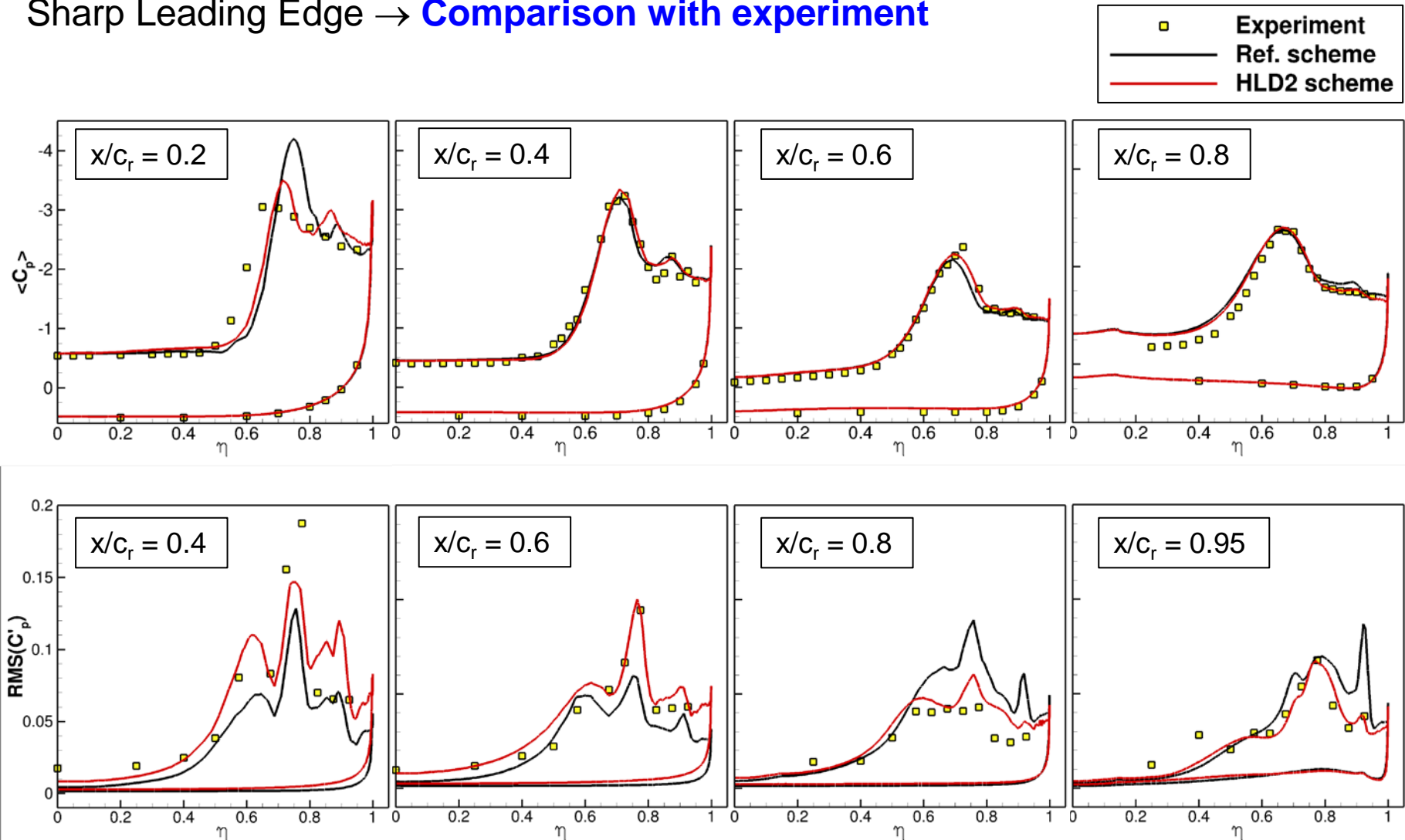


 HLD2  
sensor:



# Hybrid RANS/LES results for VFE-2 Delta Wing at $\alpha = 23^\circ$

Sharp Leading Edge  $\rightarrow$  Comparison with experiment

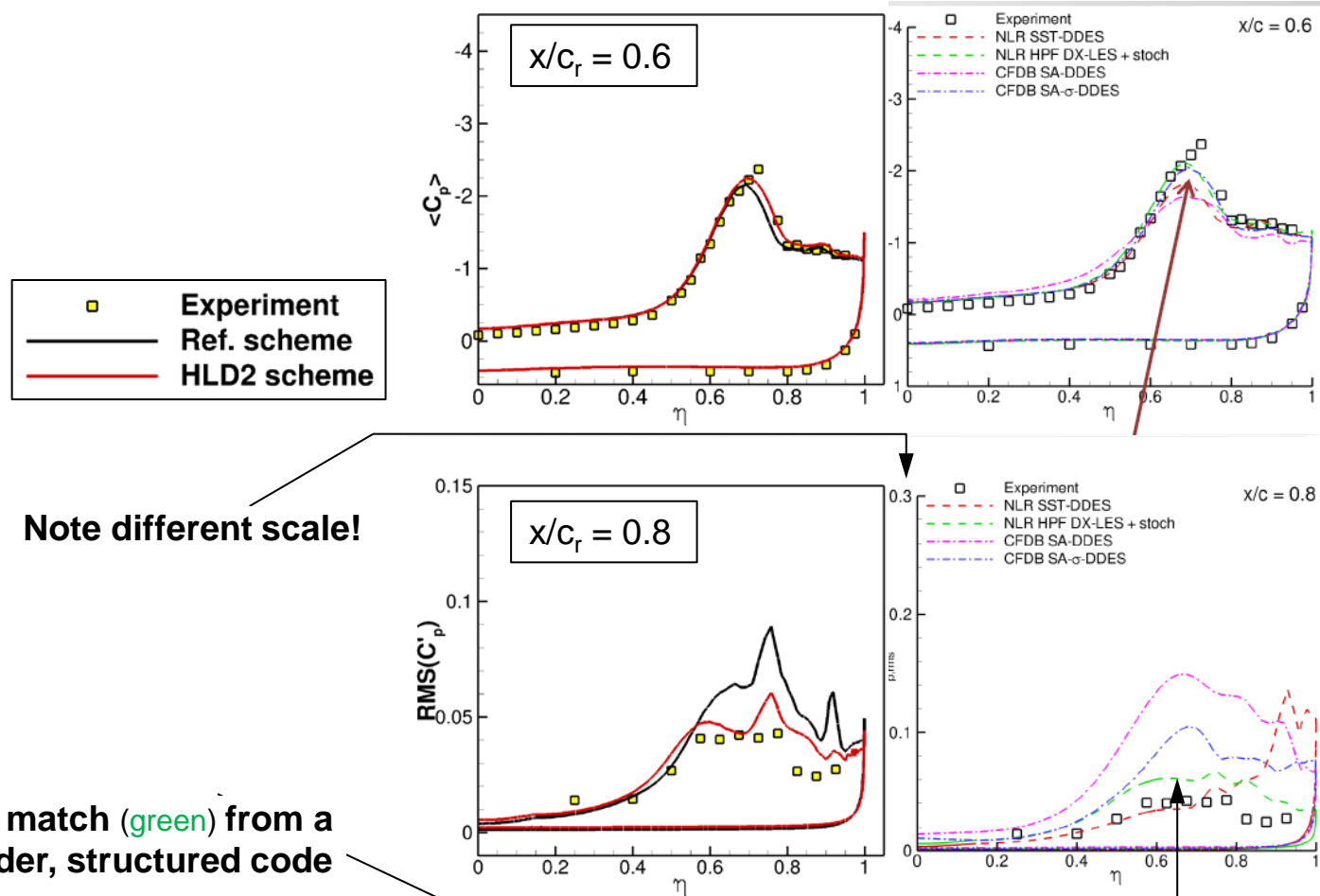




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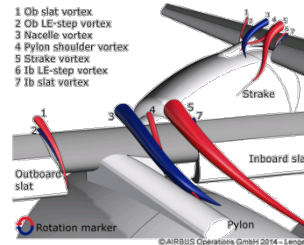
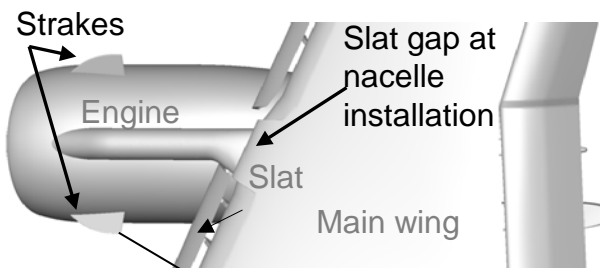
**Go4Hybrid** (EU project)  
partner results:



# Hybrid RANS/LES results for a vortex-boundary-layer interaction

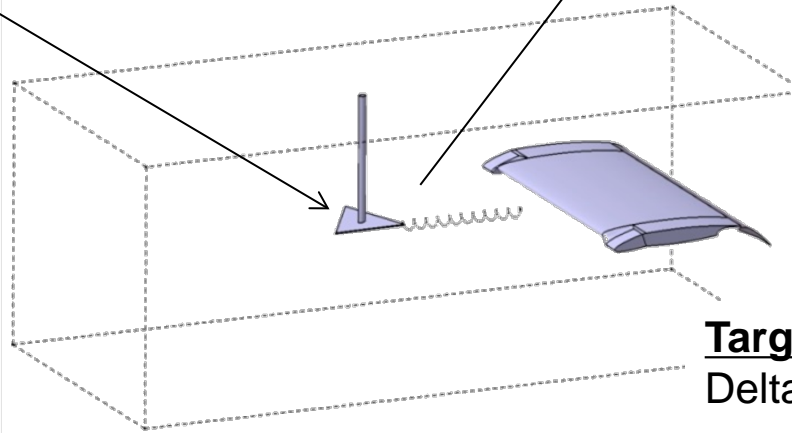
## Reality:

Wing with engine nacelle



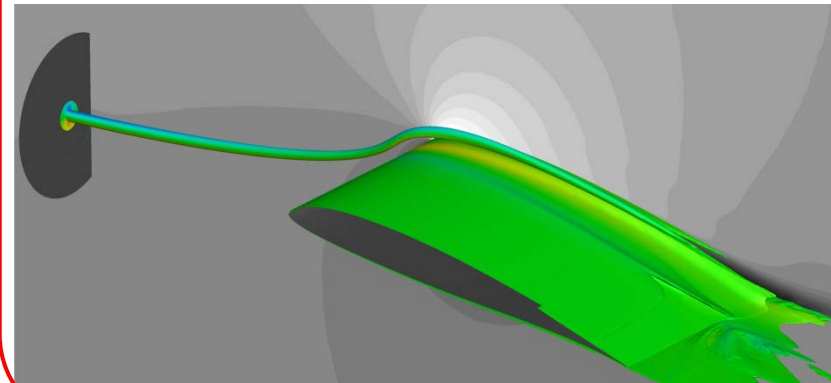
Picture from: M. Lengers;  
Industrial Assessment of  
Overall Aircraft Driven Local  
Active Flow Control

Reduction of  
Complexity  
→ Concentrate  
on relevant flow  
features



## Principal study:

Actuator disc + HGR01 single-element



Reduction of  
computational effort  
→ enable systematic  
investigations

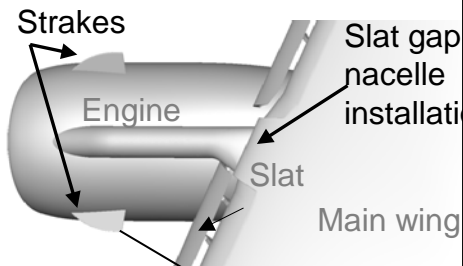
## Target configuration:

Delta wing + DLR-F15 two-element

# Hybrid RANS/LES results for a vortex-boundary-layer interaction

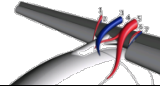
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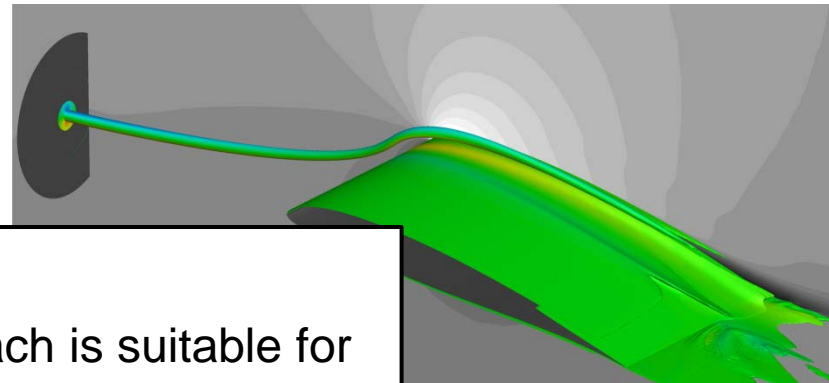
Reduction of Complexity  
→ Concentrate on relevant flow features

1 Ob slat vortex  
2 Ob LE-step vortex  
3 Nacelle vortex  
4 Pylon shoulder vortex  
5 Stroke vortex  
6 lb LE-step vortex  
7 lb slat vortex



## Principal study:

Actuator disc + HGR01 single-element



## Motivation:

- Which modeling approach is suitable for a correct representation for the vortex-boundary-layer interaction?
- Is RANS with RSM sufficient?
- Is SRS necessary?
- How must the different approaches be applied? → grid properties, time steps, CTUs, ...
- Will there be vortex burst?
- ...

Experiences in vortex simulations are currently being made

of  
onal effort  
systematic  
ons

## ation:

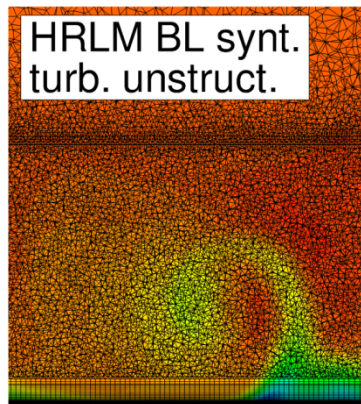
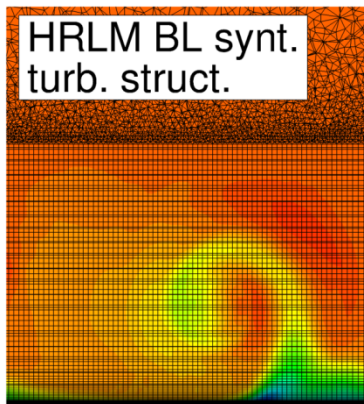
R-F15 two-element



# Hybrid RANS/LES results for a vortex-boundary-layer interaction

- Resolved structures →

- Effect of the vortex on the boundary layer at  $x/c = 0.67$



- Grid influence low

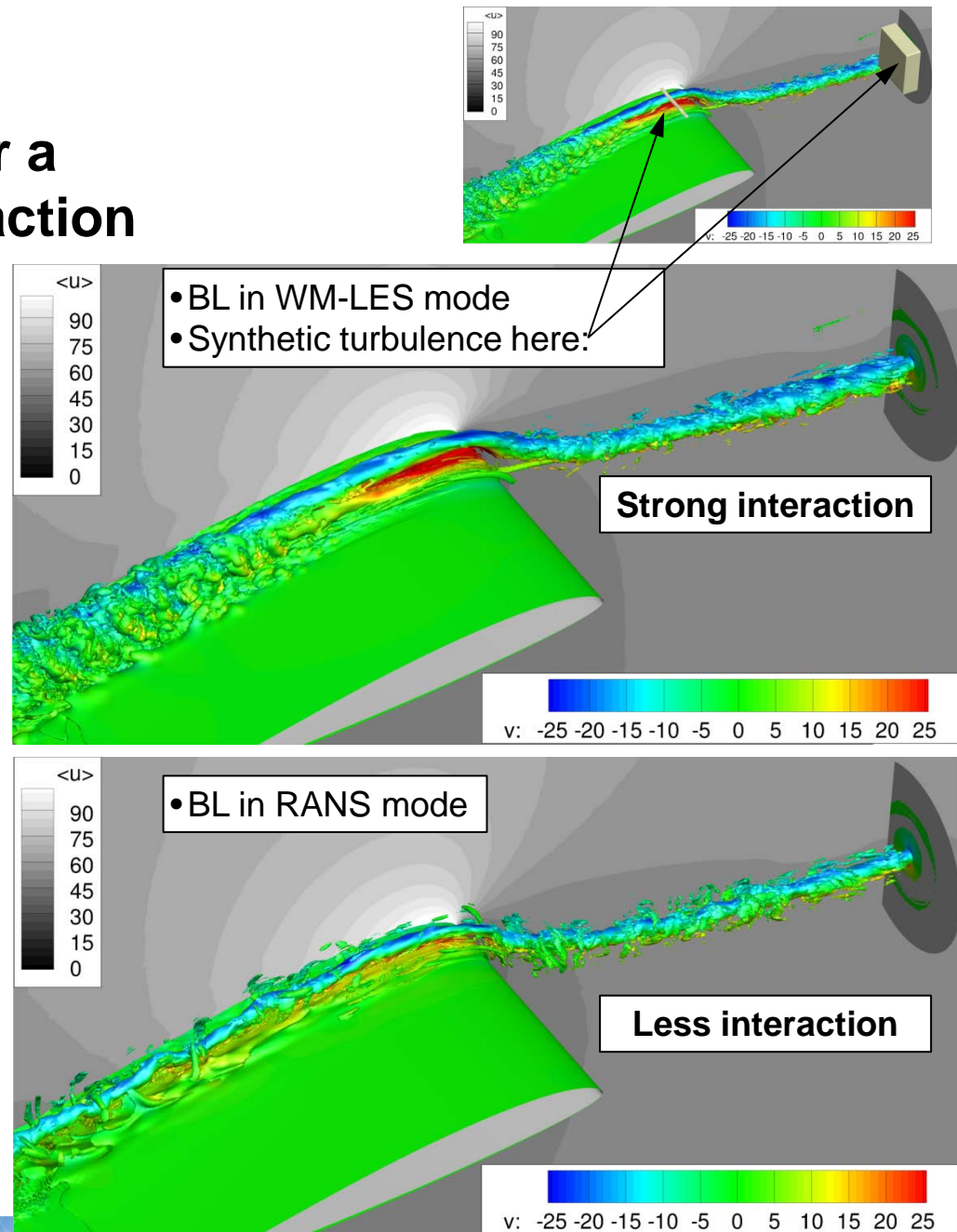


Chart: S. Probst



## WP 3: Extension a SRS approach through coupling to RSM

- Coupling of SSG/LRR to the SRS infrastructure in the TAU code
- Test computations using the most promising SRS + RSM
  - Demonstrate basic usability/functioning (from technical point of view)
  - Verification and simple validation test cases
    - ⇒ **Decision Milestone:** if this fails suggestion(DLR)/discussion how to proceed
  - Decision if  $\omega$  or  $g$  or  $\ln(\omega)$
- Selection of one SRS approach based on the results and findings from WP2
- Computation of selected test cases from WP2
- Comparison with experimental data and results from WP2

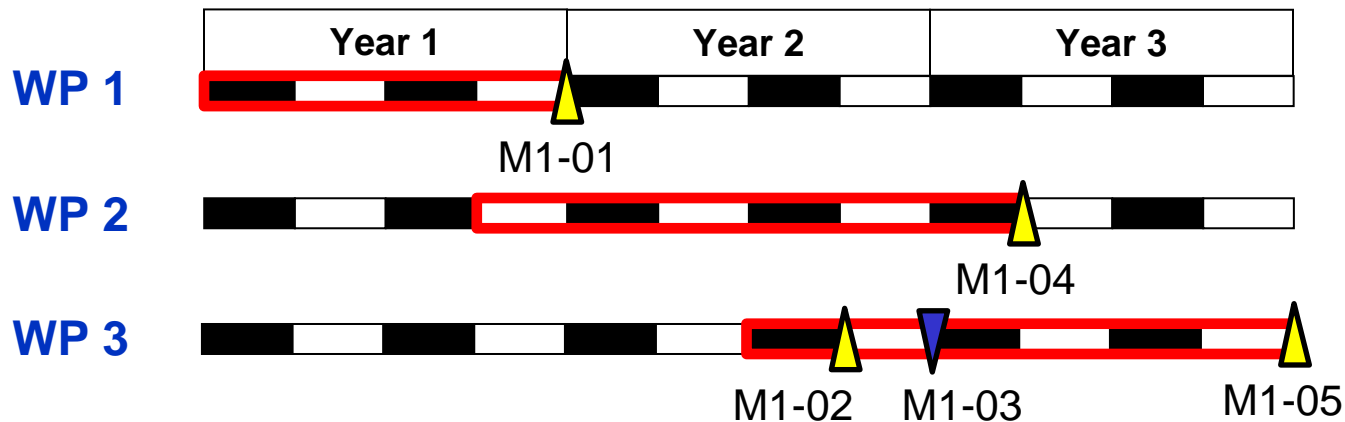
- Goals:**
- Clarification if RSM-based SRS beneficial and preferable compared to EVM-based SRS
  - Determination and classification of the advantages
  - Application recommendations, Best Practice



# Timeline & Configurations

## Milestones:

M1-01	Assessment of RSM capabilities for separated vortex-dominated flows available	QIV/Y1
M1-02	Basis SRS-RSM coupling implemented	QIII/Y2
<b>M1-03</b>	Verification of SRS-RSM coupling and simple validation test cases finalized	QIV/Y2 !!!
M1-04	Clarification which SRS approach is appropriate available	QI/Y3
M1-05	Determination and classification of advantages of SRS-RSM	QIV/Y3



## Possible configurations:

- VFE-2
- Diamond wing (NATO/STO AVT-183)
- SACCON/DLR-F17
- ...



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